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**Mech** 

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#### Heat transfer and distortion of a beamblank mold: plant measurements and model computations

Lance C. Hibbeler (MS Student)



Department of Mechanical Science and Engineering University of Illinois at Urbana-Champaign



# Objective

- Analyze a beam blank mold (Steel Dynamics, Inc.) with a numerical model to investigate:
  - Mold temperatures
  - Mold cracking
  - Thermal distortion of the mold and water box
- Incorporate the distortion results into a coupled thermal-stress model of the solidifying shell

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# **Beam Blank Mold**





# Heat Flow Into Mold

 Previous modeling work, combined with plant measurements, yields a validated heat flux profile down the mold









### **Heat Flux Validation**

	Experimental (kW)	Mold Model (kW)	Error
Wide Face	1112	1205	+8.3 %
Narrow Face	651	634	-2.6 %
Total	1764	1839	+4.3 %
3.5 3.0 2.5 2.0 1.5 0.0 0 100 200 300 Distance Re	400 500 600 700 800 9	5.0 Meniscus(1 4.5 165.1mm b 4.0 590.6mm b 3.5 Shoulder 3.0 2.5 2.0 1.5 100 00 1.5 0.0 0 00 Distance	52.4mm from top) elow top = 222.3mm below top elow top $\rightarrow$ 406.4mm below top elow top $\rightarrow$ 812.8mm below top Flange corner Narrow face $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$ $\rightarrow$



## **Other Model Parameters**

WF water channel convection coefficient	45 kW/(m²·K)
WF water temperature	33.35 °C
NF water channel convection coefficient	34 kW/(m²·K)
NF water temperature	34.48 °C
Copper thermal conductivity	350 W/(m·K)
Copper elastic modulus	115 GPa
Copper Poisson's ratio	0.33
Copper coefficient of thermal expansion	17.0·10 <sup>-6</sup> 1/ºC
Steel water box elastic modulus	200 GPa
Steel water box Poisson's ratio	0.26

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### Narrow Face Temperatures



# Hot Face Temperatures





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# Mold Cracking

• The hot spots predicted on the mold hot face in the meniscus area correspond to cracks that have occurred in practice





[D. Lorento, 2004] University of Illinois at Urbana-Champaign



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### Translating the Mold Distortion

- In the two-dimensional models of the solidifying shell, the effects of the mold changing shape with distance down the mold are incorporated with displacement functions
- The distorted shape of the mold is processed to create a displacement field relative to the shape at the meniscus
  - Double linear interpolation of the undistorted hot face *coordinates* subtracted from the distorted hot face *coordinates*







# Consortium

# Mold Distortion Results

- Mold generally bows outwards towards the shell, with a small twisting motion
- Web-region distortion is about 0.4mm, which effectively doubles the taper
- Slant region (between shoulder and inner-flange corner) distorts about 0.2mm towards the steel, which slightly lessens the negative taper
- Flange region distorts about 0.2mm, which only slightly increases the taper.
- Corner experiences negligible distortion (wellcooled)
- Narrow face distortion increases taper curvature, causing ~0.5mm more distortion at 1/3 down mold, and ~0.5mm less at bottom (causing negative taper)

## Conclusions



- Thermal distortion of a beam blank mold has been calculated, using an experimentally validated heat flux profile
- Locations on the hot face furthest away from the water channels become very hot, especially near the meniscus
  - Problem solved by more and/or smaller water channels in key areas (eg. Shoulder region)
- As the mold heats up, it generally bows outward towards the shell, with a small twisting motion, modifying the taper slightly
- The distorted shape has been successfully processed into displacement functions for use in a two-dimensional Lagrangian model of the shell

Metals Processing Simulation Lab



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Lance C. Hibbeler

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